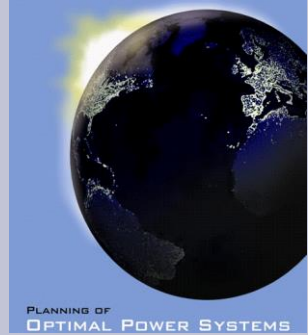


# 3. PLANNING OF POWER SYSTEM RESERVES

Asko Vuorinen

10.3.2016

Aalto University



# Reliability terms



# Reliability terms

Forced outage rate (FOR)

$$\text{FOR} = \text{FOH}/(\text{FOH}+\text{SH})\times 100 \%$$

FOH = forced outage hours

SH = service hours



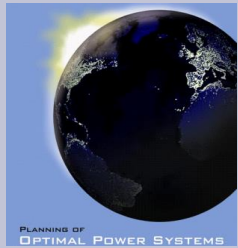
# Reliability terms, continued



Equivalent forced outage rate (EFOR)

$$\text{EFOR} = \frac{\text{FOH} + \text{EFDH}}{\text{FOH} + \text{SH} + \text{EFDH}} \times 100 \%$$

EFDH = equivalent forced derated hours  
(output reductions + forced hours)



# Reliability terms, continued

Equivalent forced outage rate demand

$$\text{EFORd} = \frac{f \times \text{FOH} + f_p \times \text{EFDH}}{\text{SH} + f \times \text{FOH}} \times 100 \%$$

$$f = (1/r + 1/T)/(1/r + 1/T + 1/D)$$

$$f_p = \text{SH}/\text{AH}$$

AH= available hours

r = average forced outage duration = FOH/number of forced outages

T = average times between calls of unit to run

D = average run time = SH/number of successful starts



# Reliability terms, continued

## Starting reliability (SR)

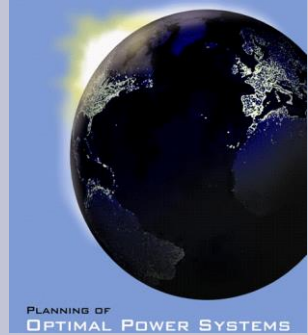
$$\text{SR} = \frac{\text{actual unit starts}}{\text{attempted starts}} \times 100 \%$$



# US Statistics (1999-2003)\*

	EFORd	SR
Conventional plants	6.2%	98.4%
- Coal-fired plants	6.4%	97.4%
- Oil-fired plants	5.7%	99.4%
- Gas-fired plants	5.9%	99.2%
Nuclear plants	5.4%	98.5%
Hydro plants	3.6%	99.5%
Combined cycles	5.6%	97.6%
Gas turbines (GT)	7.5%	95.5%
Aero-derivative GT	6.8%	97.2%
Diesel engines	5.4%	99.4%

\*Source: North American Reliability Council (NERC)



# Reliability of power system





# Probability that exactly $m$ of $n$ units are in operation



$$P(M=m|n, R) = \frac{n!}{m! (n-m)!} R^m (1-R)^{n-m}$$

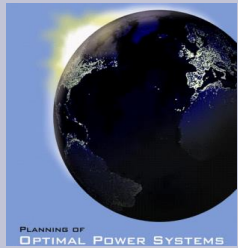
$n$  = number of units in the system

$n!$  =  $1 \times 2 \times 3 \times \dots \times n$

$m$  = number of units in operation

$m!$  =  $1 \times 2 \times 3 \times \dots \times m$

$R$  = reliability of an unit =  $1 - \text{EFOR}_d$



# Probability that at least m of n units are in operation



$$P(M=m|n, R) = \sum \frac{n!}{m! (n-m)!} R^m (1-R)^{n-m}$$

n = number of units in the system

$n! = 1 \times 2 \times 3 \times \dots \times n$

m = number of units in operation

$m! = 1 \times 2 \times 3 \times \dots \times m$

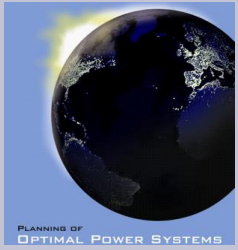
R = reliability = 1 - EFORd



# SYSTEM RELIABILITY

## $R = 95\%$ (EFORd = 5%)

n	1	2	3	4	5	10	20	50	100
n	95,0000	90,2500	85,7375	81,4506	77,3781	59,8737	35,8486	7,6945	0,5921
n-1		99,2750	99,2750	98,5981	97,7408	91,3862	73,5840	27,9432	3,7081
n-2			99,9875	99,9519	99,8842	98,8496	92,4516	54,0533	11,8263
n-3				99,9994	99,9970	99,8972	98,4098	76,0408	25,7839
n-4						99,9936	99,7426	89,6383	43,5981
n-5						99,9997	99,9671	96,2224	61,5999
n-6							99,9966	98,8214	76,6014
n-8							99,9997	99,6812	87,2040
n-9								99,9244	93,6910
n-10								99,9970	97,1812
n-11								99,9995	99,5726
n-12									99,8536

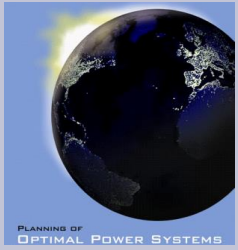


# Normal utility system\*

## Reliability target ( $R_s = 99.9\%$ )

System	Reserve need
3 x 100 %	200 %
4 x 50 %	100 %
5 x 33 %	67 %
13 x 10 %	30 %
25 x 5 %	25 %
113 x 1 %	13 %

\*Unit reliability = 95 %



# Modern utility system\*

## Reliability target $R_s = 99.99\%$



System	Reserve need
4 x 100 %	300 %
5 x 50 %	150 %
14 x 10 %	40 %
26 x 5 %	30 %
115 x 1 %	15 %

\*Unit reliability = 95 %



# Reserve margin (RM)

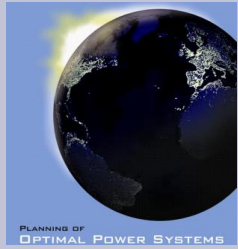
$$RM = \frac{\text{Capacity-Peak load}}{\text{Peak load}} = \frac{1 - R + Z \times \sigma/n}{R - Z \times \sigma/n}$$

R = reliability of unit

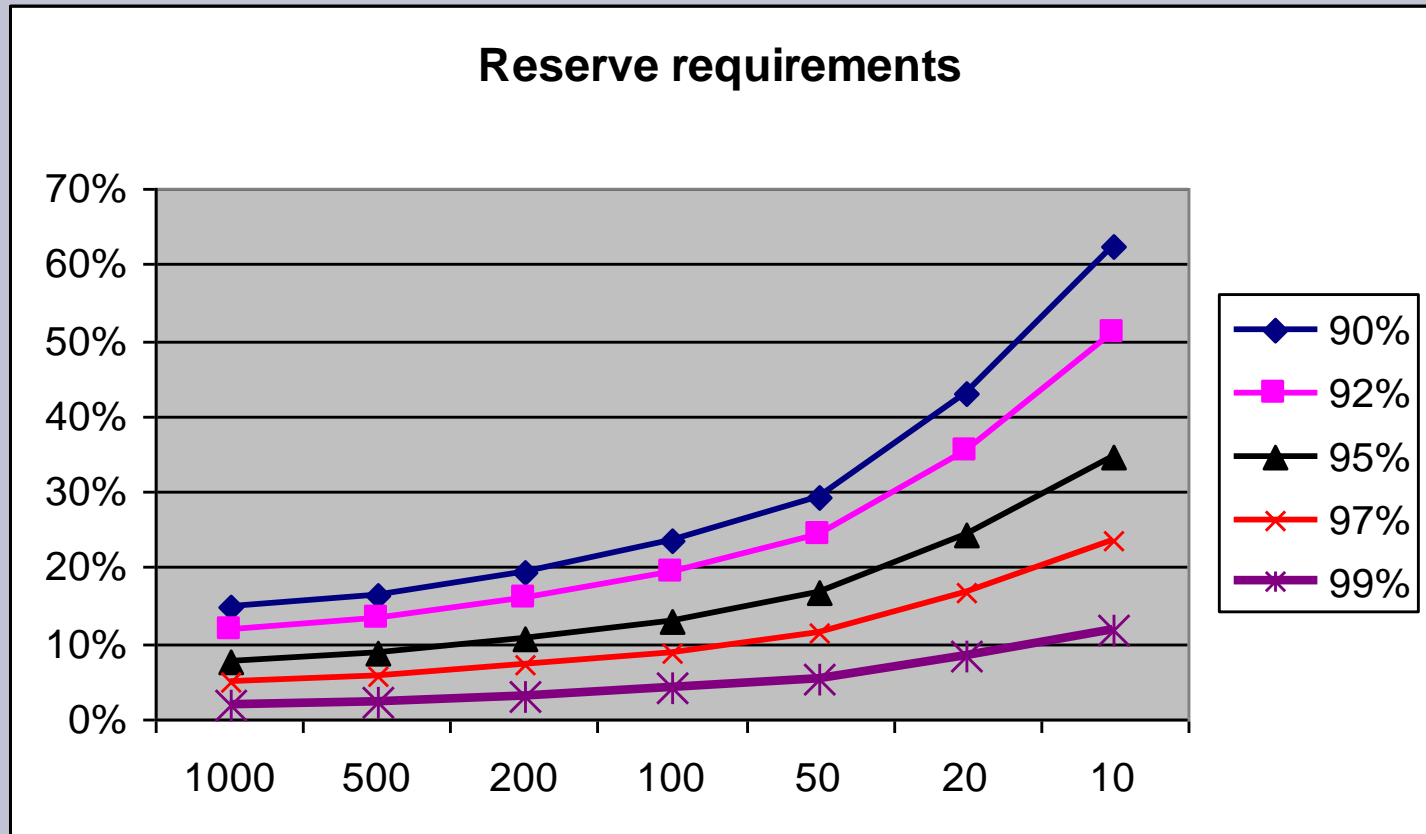
Z = level of confidence

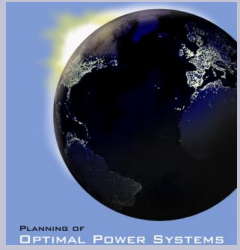
Sigma = standard deviation of reliability

n = number of units in the system



# Reserve requirements at three sigma level ( $R_s = 99.7\%$ )



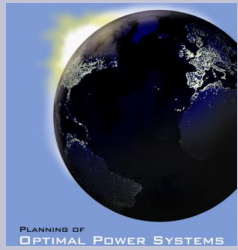


# General

Utility system needs less reserves, if the number of units ( $n$ ) will grow and if the reliability of units ( $R$ ) increases

System with 100 units needs 10 – 20 % reserves when the reliability of units varies from 92 to 97 %





# Reserve requirements with one large and several small units

## Simplified formula

$$RR = \sum ((1-R) \times P_{ui}) + P_{\max}$$

Where

RR = reserve requirement

$P_{\max}$  = largest unit in the system

R = reliability of the other units

$P_{ui}$  = output of unit i



# Reserve requirements with one large and several small units

If the largest unit is 10 % of system size and the unreliability of other units is 5 %, then

$$RR = 5 \% + 10 \% = 15 \%$$



# Optimal reliability targets

National power system = 99.9 %

Interconnected system = 99.99%

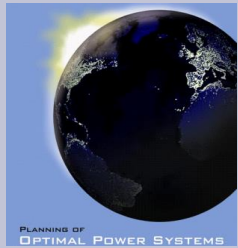
Safety related power system = 99.9999%\*

\* Can be planned by adding standby diesel engines, which start within one minute, when the interconnected system fails (see slide 12 for configurations)



# OPERATING RESERVES

- Spinning reserves
  - Synchronised reserves
- Non-spinning reserve
  - Unsynchronised reserves
- Supplemental reserves
  - 30 – 60 minute reserves
- Slow reserves
  - 1 – 12 hours reserves



# Spinning reserves

- Spinning reserves = rotating reserves act immediately by the rotating mass of the generator
- If the frequency starts dropping, the generator inertia tends to resist the slowing down motion



# Spinning reserve by Combustion Engines

- Operating power plants which can change their output by  $\Delta P$  in  $\Delta t$ 
  - Ten minute spinning reserves in USA ( $\Delta t = 10$  min)
- CEs change their output from 40 % to 100 % in ten minutes

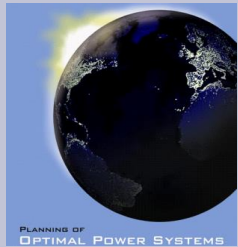


# Non-spinning reserves

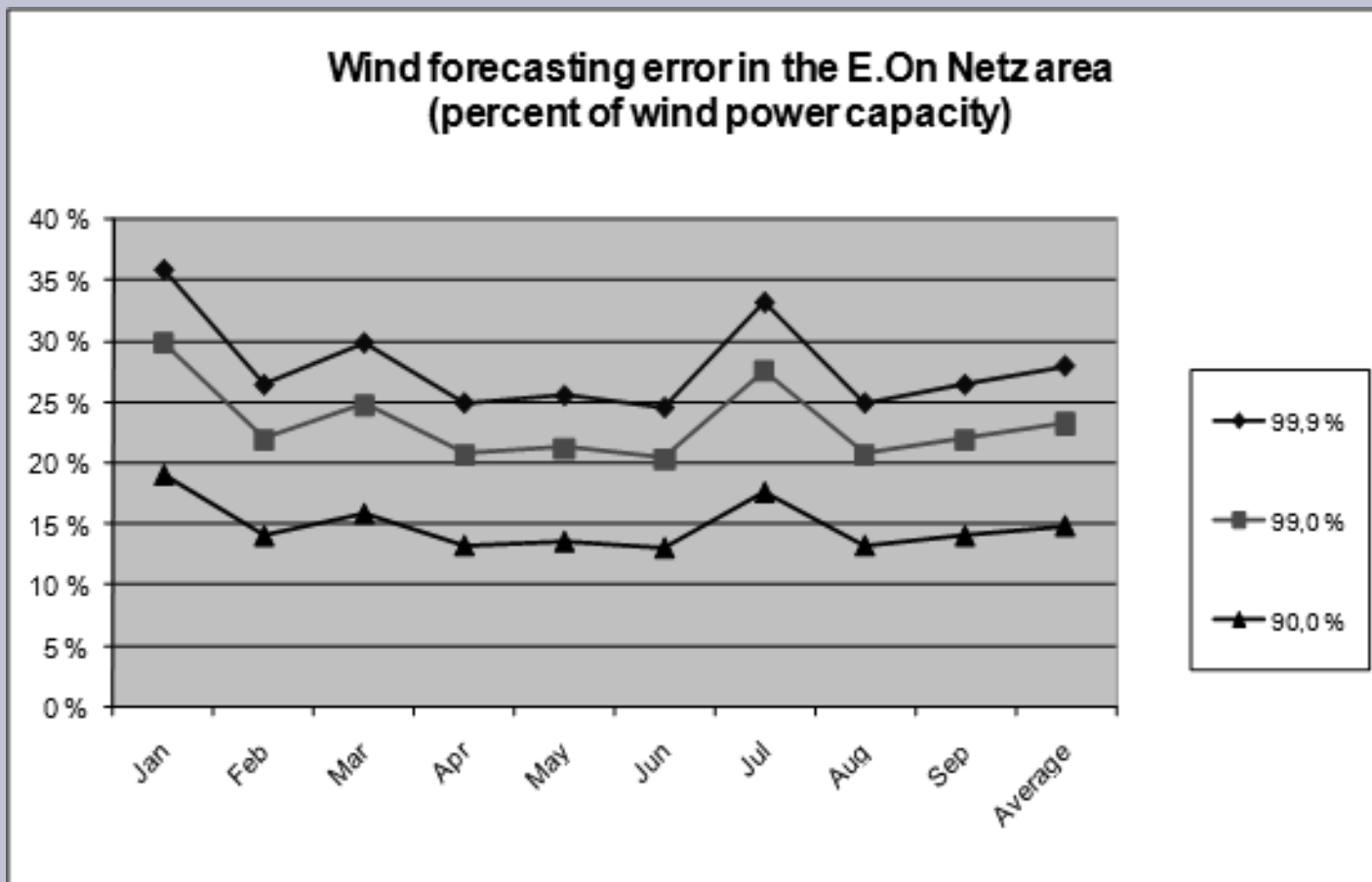
Power plants, which can start up in  $\Delta t$  minutes to full output  $P$

- Ten minute non-spinning reserves in USA ( $\Delta t = 10$  min)

- Fast reserves in UK ( $\Delta t = 5$  min) and Nordel ( $\Delta t = 15$  min)

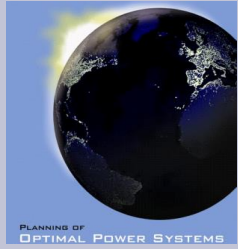


# Wind power forecasting errors and need for reserves



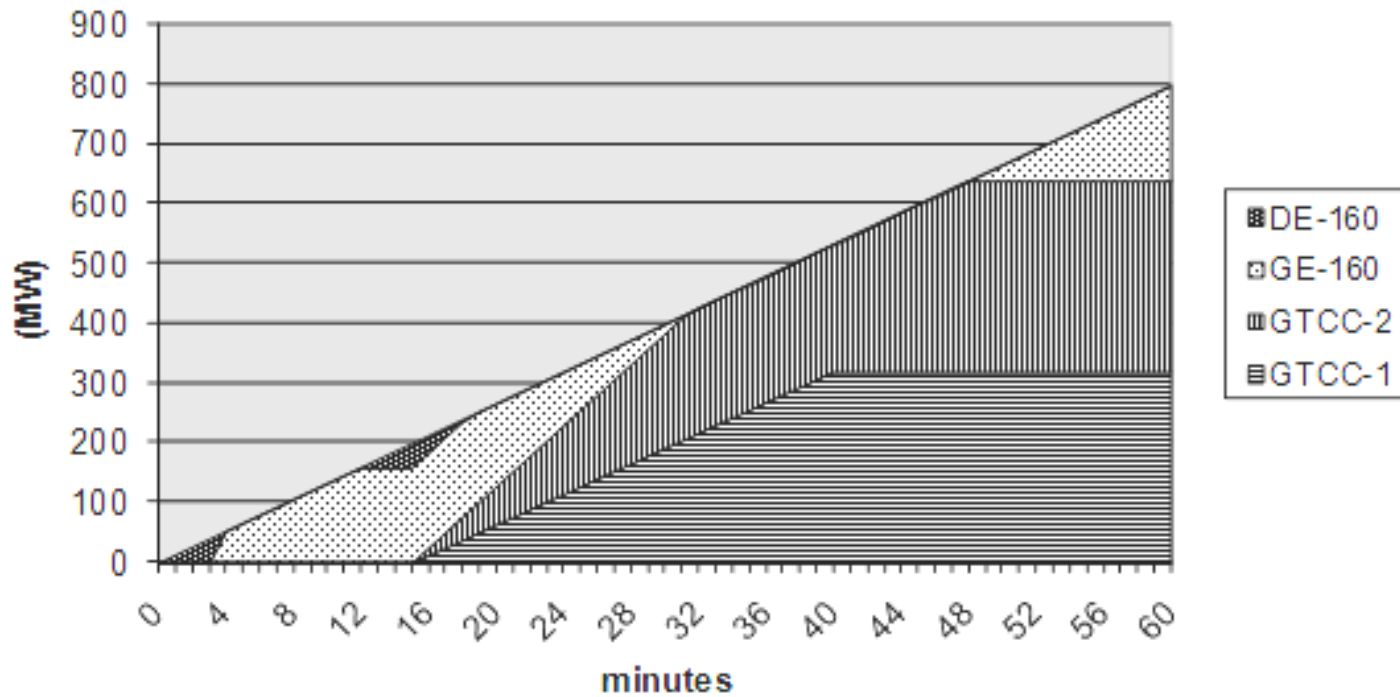
Maximim error is 28% from the installed wind capacity

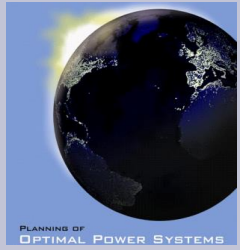




# How to compensate 800 MW drop of wind power?

Balancing the decrease of wind power with oil and gas fired power plants





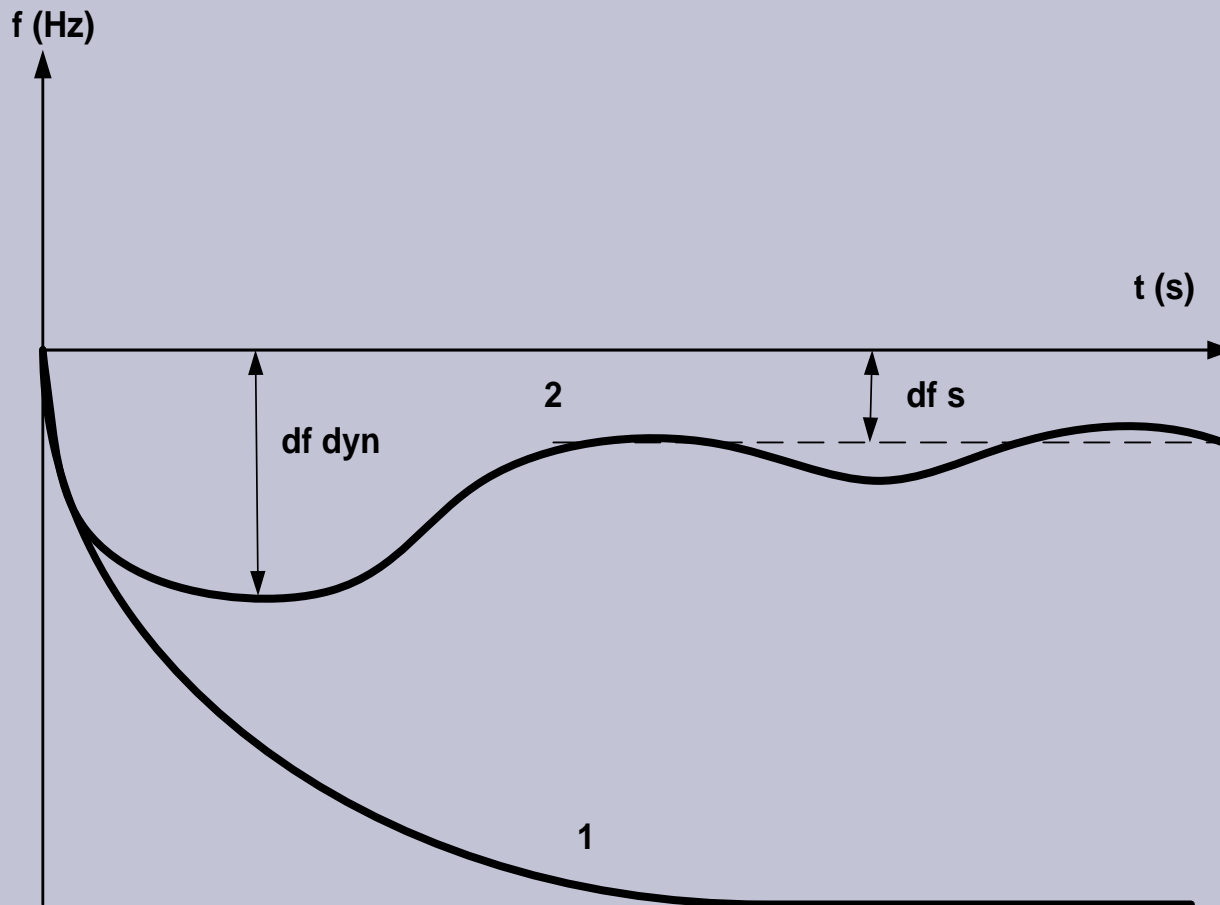
# 220 MW Plains End Plant in Colorado (2001 20 x 5,5 MW+2005 12 x 8 MW)



Bild to compensate 1000 MW wind power variations



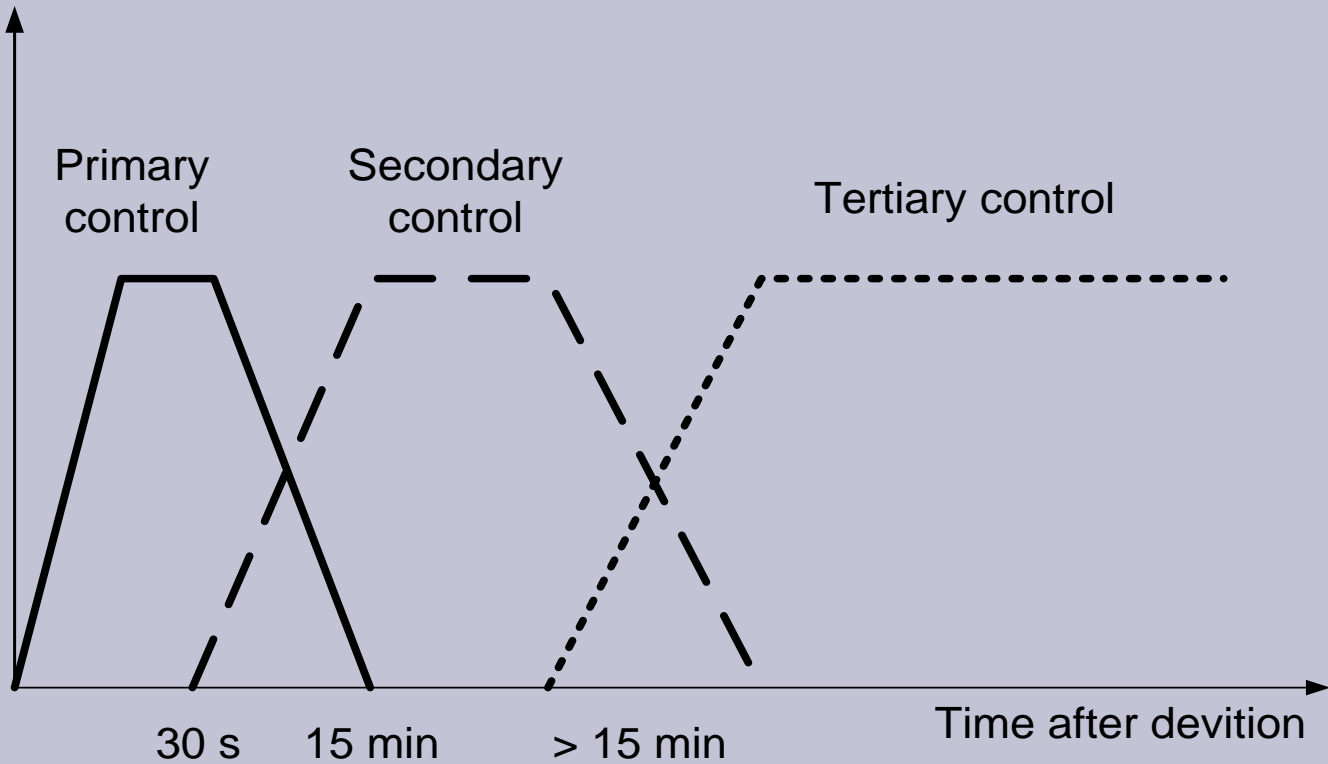
# How to compensate a trip of 1600 MW nuclear plant?





# A trip of a 1600 MW nuclear plant

● ● ● Power (MW)





# Fast Actions Needed

## Primary control

Spinning reserves should act within 30 seconds

## Secondary control

Non-spinning and spinning reserves should restore spinning reserves within 15 minutes

## Tertiary control

Supplementary reserves should restore secondary control within 30 to 60 minutes



# Secondary Control

$$dP = -K \times ACE - 1/Tr \int ACE dt *$$

where

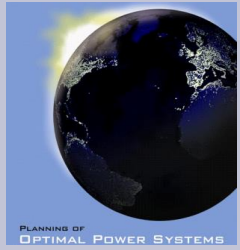
$dP$  = output set point of secondary controller

$K$  = gain of P – controller

$ACE$  = Area Control Error

$Tr$  = time constant of secondary controller

\* Note: The control action  $dP$  increases by integral formula, if the deviation of  $ACE$  remains constant (PI-type controller)



# ACE = Area Control Error

$$ACE = dB + K \times df$$

Where

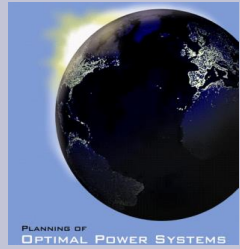
$dB$  = deviation in power balance (= Generation-Load + Import - Export)

$df$  = deviation of frequency from ( $f_N$ )

$K$  = dependency between deviation of power and system frequency

Note: ACE is calculated in ten second intervals by computers in the dispatch center in USA

If  $ACE >$  given limit, penalties will be given to utilities

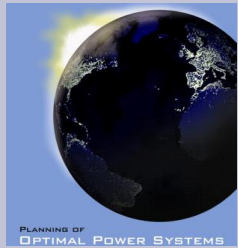


# 250 MW non-spinning reserve plant Kiisa , Estonia



Includes 27 Wärtsilä 34DF 10 MW engines





# Black-start diesel generators

Emergency Diesel Generators (EDG)

Station Blackout Diesel Generators  
(SBO)



# Starting reliability (SR=97 %)

n	1	2	3	4	5	6	7	8	100
n	97,0000	94,0900	91,2673	88,5293	85,8734	73,7424	54,3794	21,8065	4,7553
n-1		99,7354	99,7354	99,4814	99,1528	96,5493	88,0162	55,5280	19,4622
n-2			99,9973	99,9894	99,9742	99,7235	97,8992	81,0798	41,9775
n-3				99,9999	99,9996	99,9853	99,7331	93,7240	64,7249
n-4						99,9995	99,9980	98,3189	81,7855
n-5							99,9999	99,6264	91,9163
n-6								99,9296	96,8772
n-8								99,9886	98,9376
n-9								99,9984	99,6784
n-10								99,9998	99,9126
n-11									99,9785
n-12									99,9952



# Emergency Diesel Generators (EDG) in Nuclear Plants

Single Diesel Generator

1 x 100 %,  $R > 0.9700$

American nuclear plants

2 x 100 %,  $R > 0.9974$

Finnish and German Nuclear plants

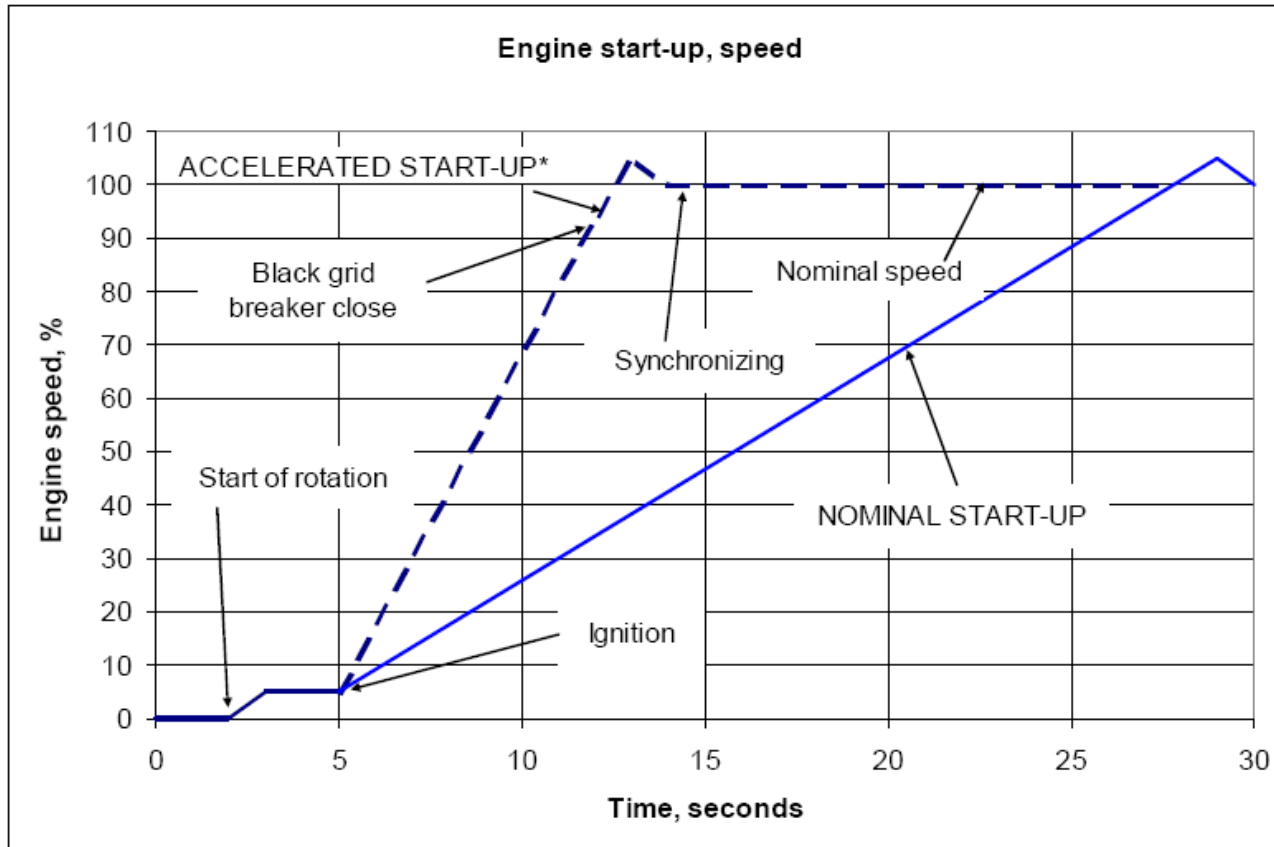
4 x 50 %,  $R > 0.9989$

One of four will start with probability

4 x 100 %  $R > 0.999999$

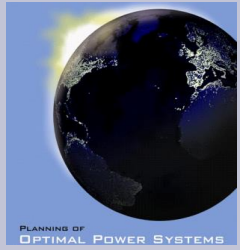


# EDG Start-up time



\* Accelerated start-up criteria:

- engine must be pre-heated
- visible smoke may occur
- not possible with engine driven fuel pump
- start air pressure must be a minimum of 28 bar



# Loviisa 10 MW SBO/Fast Reserve Diesel plant





# Need for Diesel Generators and Fast Reserves



Emergency Diesel (EDG) 4 x (3 – 8 MW)

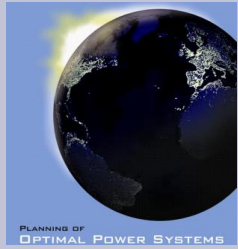
Swing Diesels (SDE) 1 x (3 – 8 MW)

Station Blackout (SBO) 1-2 x (1 – 10 MW)

Fast reserve capacity 1,18 x largest unit

1,18 x 1700 MW = 2000 MW

in Finland



# Investment costs

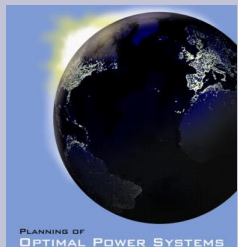
● ● ● Reserve diesel generator plant	600-700 €/kW
Gas engine CHP plant	700-800 €/kW
EDG plant	1000 -2000 €/kW
Coal or peat CHP plant	1000-1500 €/kW
Wind power park	1000-1500 €/kW
Nuclear plant	4000-6000 €/kW



# SUMMARY

- Reserve needs become lower by planning systems with smaller and more reliable units
- Largest unit determines the need of reserve capacity, if the unit sizes are unevenly distributed
- The modern electronic age requires higher system reliability figures because everything depends on computers





For details see reference text book  
**”Planning of Optimal Power Systems”**



Author:  
**Asko Vuorinen**

Publisher:  
**Ekoenergo Oy**

Printed:  
**2008 in Finland**

Further details:  
**[www.ekoenergo.fi](http://www.ekoenergo.fi)**

